

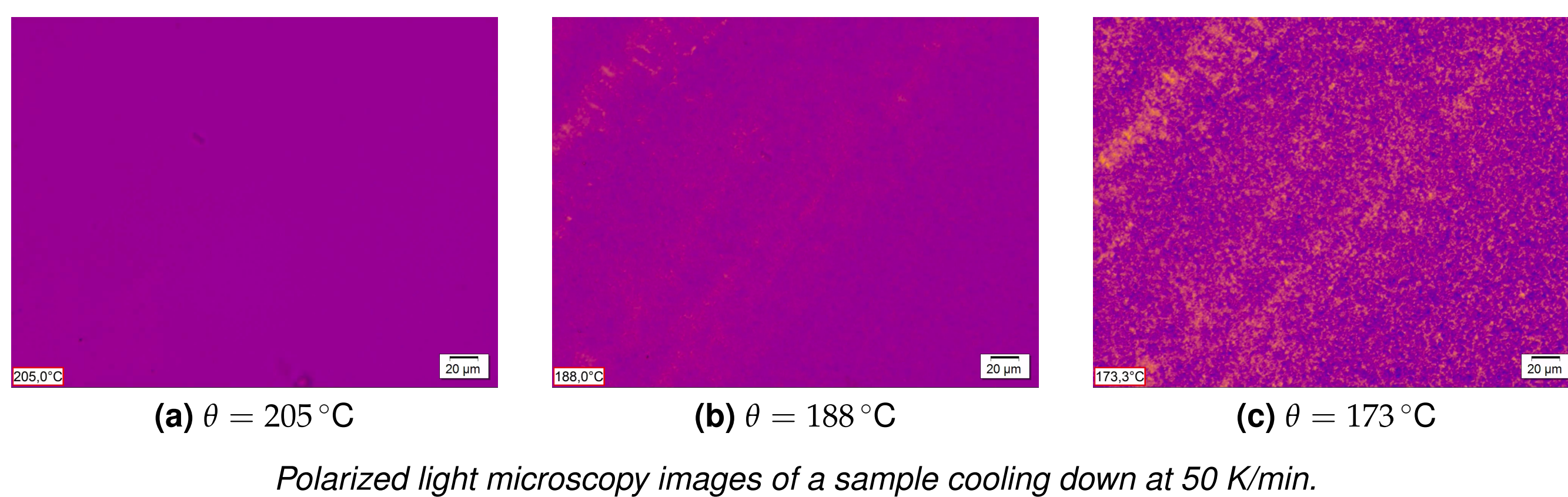
Phase-field modeling of microstructure evolution during polymer solidification

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Motivation

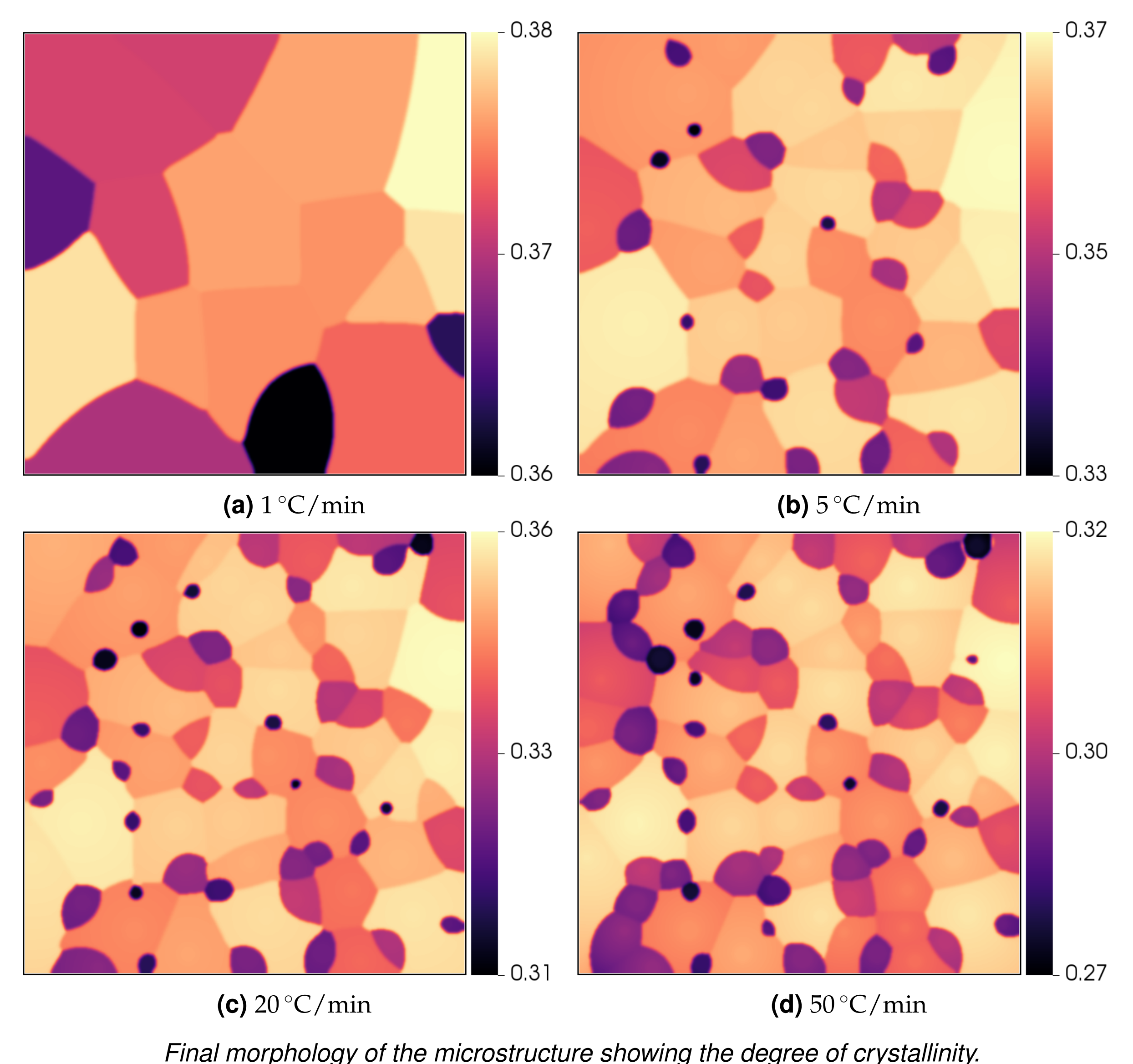
- Coarse-grained model of crystallinity morphology on the meso-scale
- A semi-crystalline phase does not represent a singular spherulite but rather a collection of spherulites, quantified by the degree of crystallinity.



Simulation of crystallinity evolution in a small domain

Initial and Boundary conditions

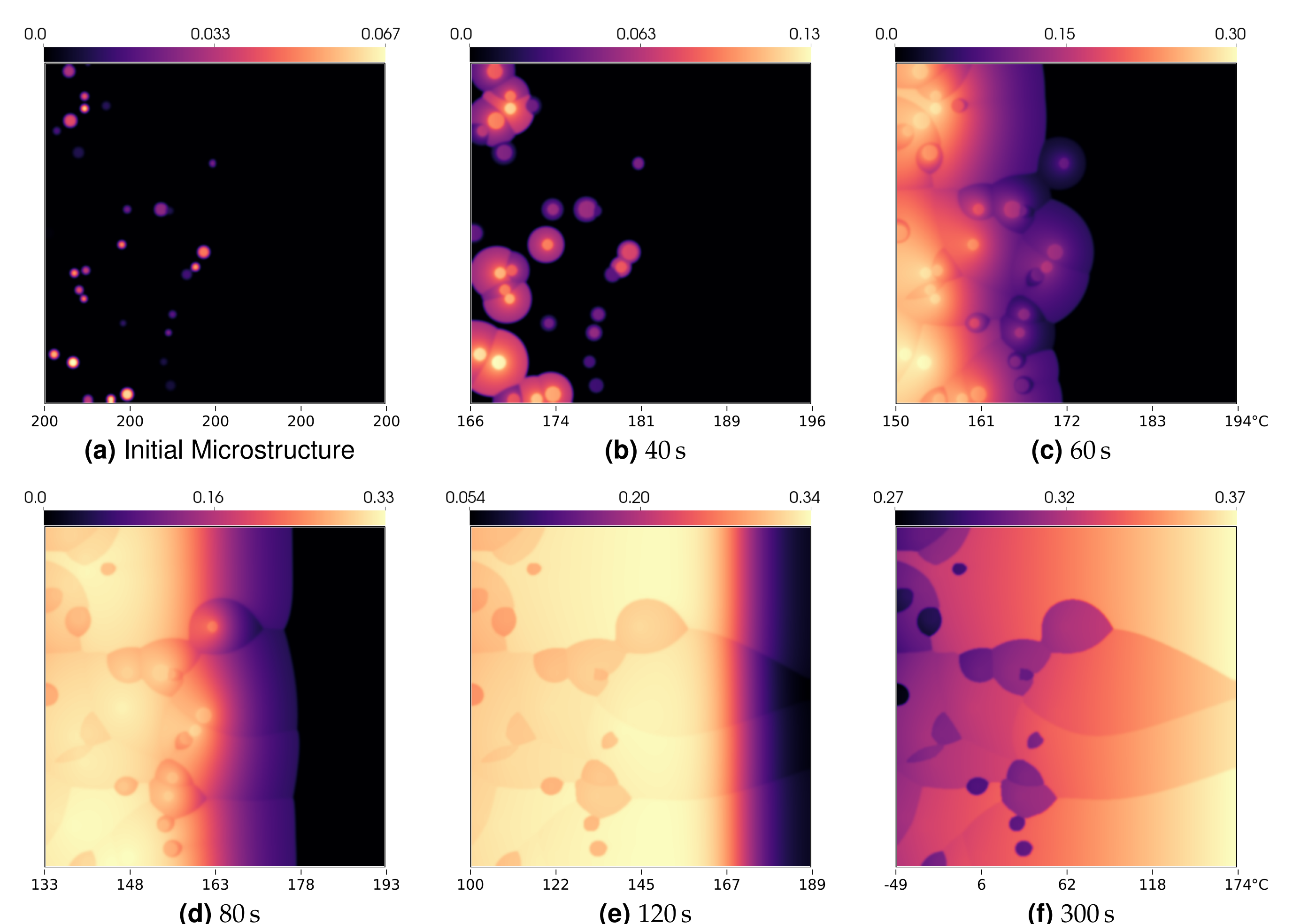
- 2D domain grid of 500×500 cells with $\Delta x = \Delta y = 1 \mu\text{m}$
- 100 randomly dispersed grains within an amorphous matrix, radii: 4–10 μm
- Initial crystallinity: randomly assigned between 0.6 % and 7 %
- Dirichlet boundaries with cooling rates $R \in \{1, 5, 20, 50\}^\circ\text{C/min}$



Effect of temperature and cooling rate gradients

Initial and boundary conditions

- 2D domain grid of 500×500 cells with $\Delta x = \Delta y = 1 \mu\text{m}$
- Grains are initialized on the left half of the domain
- Left boundary: 50°C/min , Right boundary: 5°C/min



Governing Equations

- Helmholtz free energy of the system

$$\psi^\alpha = \psi_\chi^\alpha(\chi_\alpha, \theta) + \psi_\theta^\alpha(\theta)$$

$$\psi_\chi^\alpha = \Delta h_{f,\alpha}^{100} \frac{\theta - \theta_{on,\alpha}}{\theta_{on,\alpha}} \chi_\alpha, \quad \psi_\theta^\alpha = \int_{\theta_{on}}^\theta c_{p,\alpha}(\chi_\alpha, \tilde{\theta}) d\tilde{\theta} - \theta \int_{\theta_{on}}^\theta \frac{c_{p,\alpha}(\chi_\alpha, \tilde{\theta})}{\tilde{\theta}} d\tilde{\theta}$$

- Multiphase-field model

$$\mathcal{F}[\phi, \nabla \phi, \chi] = \int_V f dV = \int_V f_{\text{grad}}(\phi, \nabla \phi) + f_{\text{pot}}(\phi) + \bar{f}_{\text{bulk}}(\phi, \chi) dV$$

$$\frac{\partial \phi_\alpha}{\partial t} = -\frac{1}{\epsilon N^*} \sum_{\alpha \neq \beta} M_{\alpha\beta} \left(\frac{\delta \mathcal{F}}{\delta \phi_\alpha} - \frac{\delta \mathcal{F}}{\delta \phi_\beta} \right)$$

- Polymer Crystallization Model

$$\frac{\partial \chi_\alpha}{\partial t} = n_\alpha K_\alpha(\theta, \dot{\theta}) (1 - \chi_\alpha) \left(\ln \left(\frac{1}{1 - \chi_\alpha} \right) \right)^{(n_\alpha - 1)/n_\alpha} \frac{\Delta h_{m,\alpha}(\dot{\theta})}{\Delta h_{f,\alpha}^{100}}$$

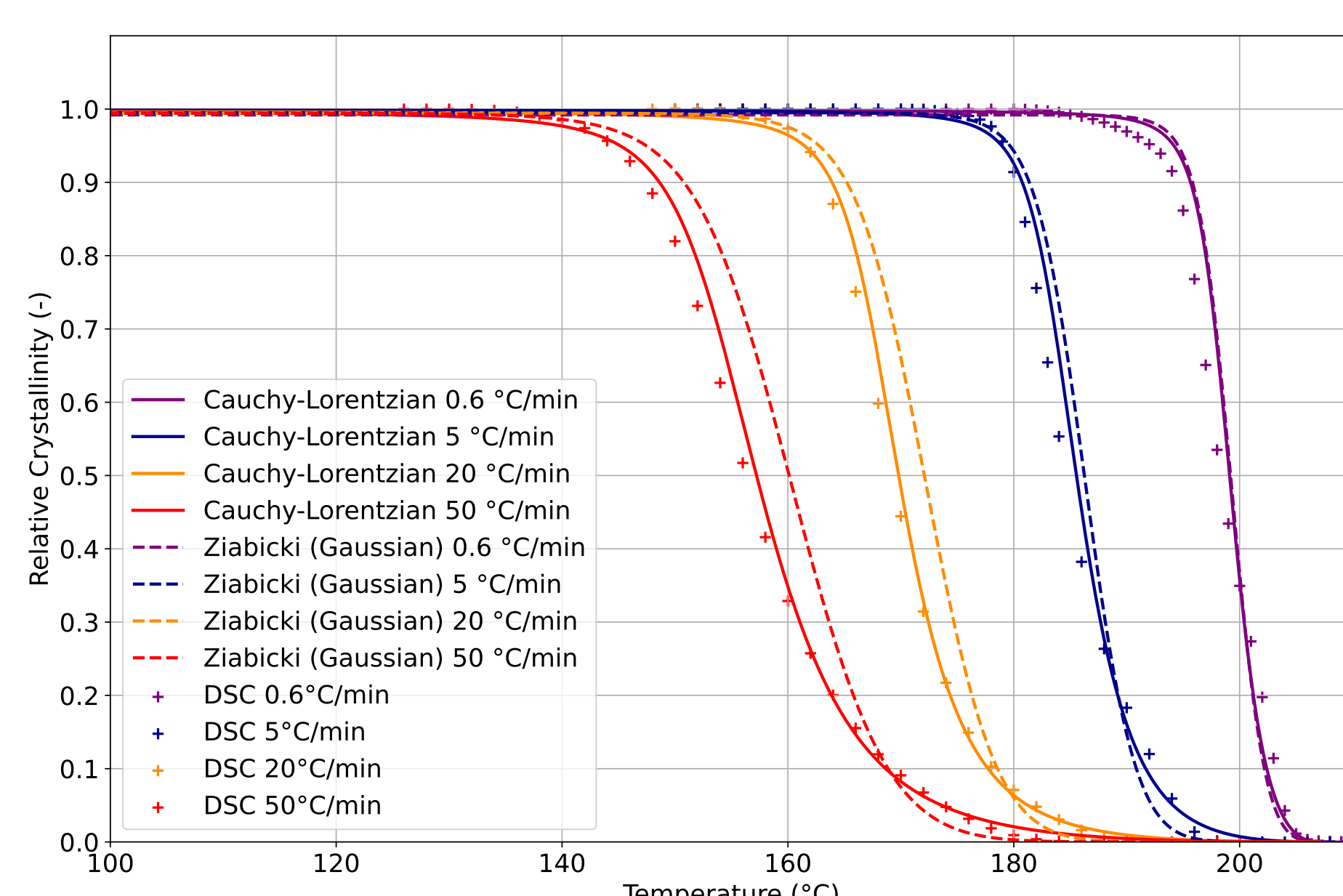
$$K_\alpha(\theta, \dot{\theta}) = K_{max,\alpha}(\dot{\theta}) \exp \left(-4 \ln(2) \frac{(\theta - \theta_{max,\alpha})^2}{D_\alpha^2} \right)$$

- Heat conduction equation

$$\bar{\rho} \bar{c}_p \dot{\theta} = -\text{div}(\bar{q}) + \underbrace{\sum_\alpha \rho_\alpha \Delta h_{f,\alpha}^{100} \dot{\chi}_\alpha \phi_\alpha}_A + \underbrace{\sum_\alpha \rho_\alpha \Delta h_{f,\alpha}^{100} \dot{\phi}_\alpha \chi_\alpha}_B - \underbrace{\sum_\alpha \dot{\phi}_\alpha \rho_\alpha \int_{\theta_{on}}^\theta c_{p,\alpha}(\chi_\alpha, \tilde{\theta}) d\tilde{\theta}}_C$$

Comparison of different formulations for K_α

- Cauchy-Lorentzian formulations offers a better fit for this sample



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